Tool- and pattern-dependent spatial variations in silicon deep reactive ion etching

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Coping with spatial variation in DRIE

- Why non-uniformity is a problem
- Controlling uniformity with the mask design
- Characterizing tools' performance
- Wafer-to-wafer effects
- Improving the mask design process

Non-uniformity problems in MEMS

Aim: remove imbalance in MIT Microengine rotor



e.g.: A.H. Epstein et al., Proc. Transducers '97

Non-uniformity problems in MEMS

also: embossing stamp fabrication for microfluidics manufacture

Si stamp



perhaps too: avoiding footing during SOI etch-through

Inductively-coupled plasma in DRIE chamber



Time-multiplexed 'Bosch' processing



Journal of The Electrochemical Society, 146 (1) 339-349 (1999); Robert Bosch GmbH, Pat. 4,855,017 and 4,784,720 (USA) and 4241045C1 (Germany) (1994)

Non-uniformity at three length scales



Strategies for improving uniformity

- Force etching to be reaction-limited
 - Lower chamber pressure
 - Wafer cooling
- Conservative mask design
- Improved tool design



- Relate mask design directly to non-uniformity
 - Design mask according to desired uniformity
 - Perturb etch rates constructively



Non-uniformity at three length scales



Previously observed chamber-scale variation



Non-uniformity at three length scales



Previously observed pattern-dependent variation



Average pattern density 5% throughout Localized to differing extents

A two-level model, tuned for each tool + recipe



H. Sun et al., Proc. MEMS 05 + work submitted for publication

Basis for chamber-scale model?



$$C = \frac{G\tau}{\underset{1}{\alpha_{1}\tau[\rho + \alpha_{2}(1 - \rho)] + 1}}$$
rate ct. selectivity 'loading'

Synergism model: Gottscho *et al.*, *J Vac Sci Tech B* **10** 2133 (1992). Right: H.K. Taylor *et al.*, submitted for publication

 $R = v S_0 (1 - \Theta) J_n$

 $\frac{1}{R} = \frac{1}{kE_i J_i} + \frac{1}{vS_0 J_n}$

mask

silicon

Basis for chamber-scale model?





Assuming:

- ion flux independent of etched pattern
- F generation (G) independent of etched pattern
- neutral flux $(J_n) \propto F$ concentration
- F concentration depleted as loading increases
- F concentration depends on G

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Accounting for spontaneity in Si etching



Accounting for time-multiplexing



Time-multiplexing model

 R_{Si} is the etch rate our previous model would have predicted. Overall, modified rate prediction:

$$R' = \frac{T_{Si-etch}R_{Si}}{T_{tot}} = \frac{R_{Si}\left(T_{etch} - T_{strip}\right)}{T_{tot}} = \frac{R_{Si}\left(T_{etch} - \frac{T_{pass}k_{pass}J_{CF_x}}{J_ik_{strip}}\right)}{T_{tot}}$$

If we define $a = T_{etch}/T_{tot}$, $p = J_i k_{strip}$, $q = k_{pass}J_{CFx}$, we have:

$$R' = \frac{\left[a(p+q)-q\right]R_{Si}}{p}$$

R' = ma + c with $m = (p + q)R_{Si}/p$ and $c = -qR_{Si}/p$.

Rate of passivation removal



(Short-term) memory effect in chamber



Thermal diffusivity of aluminum ~ 10⁻⁴ m²/s

Over 5', characteristic length ~0.17 m

Over 30', characteristic length ~0.42 m

(Short-term) memory effect in chamber



Pattern component of memory effect?



Pattern component of memory effect?



Putting two-level model into action



CAD tool for nonuniformity prediction



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